Appl. No. 09/943,589

Amdt. Dated October 20, 2003

Reply to Office Action of June 18, 2003

## SPECIFICATION AMENDMENTS

On page 9, please replace the paragraph starting on line 19 with the following amended paragraph:

A voltage signal [[Is1]] or current signal Us1 can be tapped off at the current sensing resistor RS, which voltage signal is proportional to the current sense current  $I_{\text{s}}$  or the load current  $I_{\text{L}}$  of the load transistor T1.

On page 10, please replace the paragraph starting on line 5 with the following amended paragraph:

Current sense arrangements like those produced from the circuit arrangement of the evaluation circuit BL1 according to figure 3 and the current sensing resistor T2 function with sufficient accuracy, that is to say supply a voltage signal [[Is1]] or current signal Us1 which is proportional to the load current  $I_L$ , only when the load transistor T1 is not yet in saturation, in other words as long as the load current  $I_L$  rises proportionally to the drain-source voltage UDS1.

On page 12, please replace the paragraph starting on line 5 with the following amended paragraph:

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The first evaluation circuit BL1 supplies a signal Us1 proportional to the load current  $L_L$  as long as the load transistor T1 is not yet in saturation or as long as the drain-source voltage UDS1 is less than the reference voltage ref. If the drain-source voltage UDS1 exceeds the reference voltage Uref, then the load current Is of the current sensing transistor T2 flows into the second evaluation circuit BL2, where this load current  $I_s$  generates across the second resistor R2 a voltage drop Us2 which can be used as second current signal Us2 for setting the drive voltage (gate-source voltage) of the load transistor T1. The load current of the load transistor T1 and thus also the load current of the current sensing transistor T2 are greatly dependent on the gate-source voltage in the saturation region. Depending on the load current of the current sensing resistor T2, the gate-source voltage of the load transistor can then be set by way of the current signal Us2. The second drive circuit BL2 may be used, in particular, as part of a current limiting circuit which reduces the gate-source voltage of the load transistor T1 if the load current exceeds a predetermined value, which can be determined from the voltage signal Us2.